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LASSEN COUNTY DEPARTMENT OF PLANNING AND BUJILDING SERVICES

DRAINAGE REPORT

GEOFORTIS MINERALS, LLC US 395 HAUL ROAD

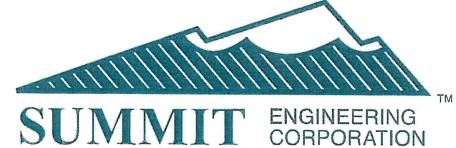
US 395 CALTRANS ENCROACHMENT PERMIT

File No. 30758

Prepared for:

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Prepared by:



February 25, 2019

No. 33629 Exp. 6-30- ZO

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Geofortis Minerals, LLC Pozzolan Mine Haul Road US 395 Encroachment Permit Drainage Study

Introduction

Geofortis Minerals, LLC is a supplier of natural pozzolans to the western United States. The company currently owns a pozzolan mine located approximately 6 miles north of Hallelujah Junction on US 395 north, just west of the highway, more specifically located within the SW and SE quarters of Section 11 and the NW and NE quarters of Section 14 within Township 23 North, Range 17 East. Currently, there is access from the mine site to US 395 from the west.

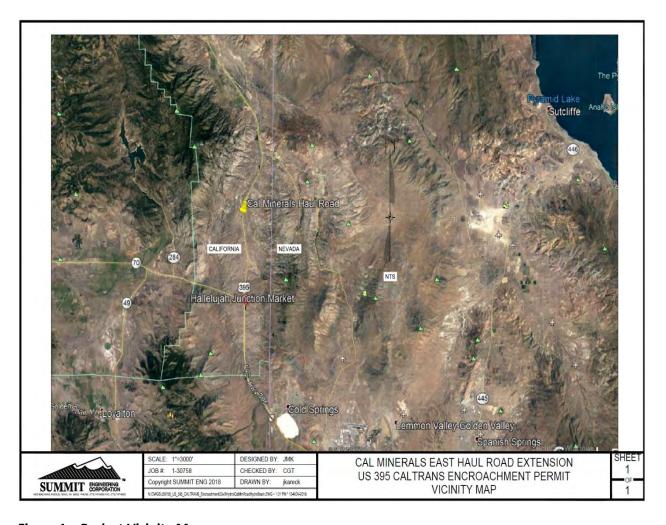


Figure 1 – Project Vicinity Map

Geofortis Minerals is proposing to mine a new area to the east of US 395 very near the intersection of the existing haul road and US 395. Proposed improvements will encompass the extension of the existing access (west of US 395) to the east side of US 395 (East Haul Road). Improvements include extending the existing road to the east of US 395 incorporating storm drain improvements. Storm drain improvements will need to perpetuate existing flows from the upper basin upstream and east of the project site. Refer to the Project Grading Plan, Attachment A.

Existing Conditions

The existing road from the mine site's former and historic processing area is currently unpaved and varies in width from 15 to 25 feet to a point approximately 180 feet west of US 395 N. From this point, the road is paved to the highway at its east extent. At and near this intersection (Caltrans Route 395 Postmile LAS 9.935), surrounding terrain is prolific with grasses, sagebrush and conifers. Upstream basin terrain ranges in slopes from 2-3% to as high as 72%.

The natural lay of the land is toward the north. Long Valley Creek runs along the west side of US 395 and drains in a northerly direction in various tributaries. Approximately 200 feet north of the proposed east haul road and US 395 intersection is an 18-inch diameter/inlet structure that diverts existing flows toward the east. The drainage flows to a ditch/tributary that runs along the east side of the highway eventually draining back to Long Valley Creek under the highway approximately a half-mile to the north.

The existing hydrology-basin mapping is provided in Attachment B. Drainage mapping indicates the area of land that contributes to the project area is approximately 5,520 acres of land, flowing in drainage ways as depicted in Attachment B. Eight (8) separate sub-basins with associated acres are also depicted in this attachment.

Soils Survey

Natural Resources Conservation Service ("NRCS") soils mapping identifies the contributing area as consisting mainly of sandy, coarse-sand and cobbly-sandy loam with areas of rock-outcroppings.

USGS Soils Mapping is provided in Attachment C. As drainage areas generally consist of loam, the hydrologic soils grouping used in the hydrology modeling is soils class A.

Analysis and Discussion

The Caltrans District 2 Hydraulics Drainage Review Requirements (dated February 25, 2006) indicates cross drains and storm drain networks within California State Right of Way are designed for the 10-year flows. The computer program utilized to model upstream basin flows for this road extension project was AutoDesk Storm and Sanitary Analysis (SSA).

National Oceanic and Atmospheric Administration ("NOAA") and the National Weather Service ("NWS") provide location information and precipitation frequency estimates as shown below:

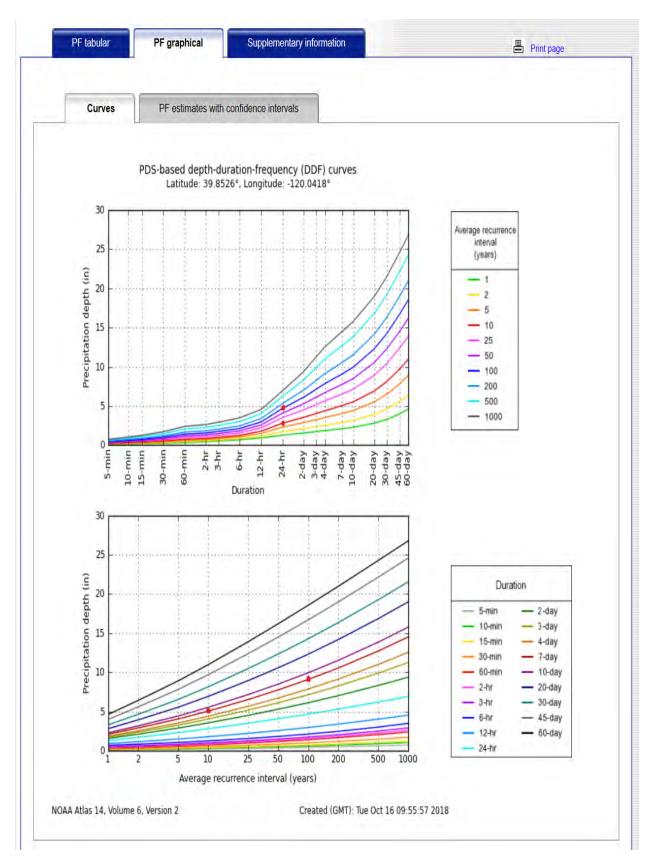


Figure 2 - Precipitation Frequency Graph

POINT PRECIPITATION FREQUENCY (PF) ESTIMATES

WITH 90% CONFIDENCE INTERVALS AND SUPPLEMENTARY INFORMATION NOAA Atlas 14, Volume 6, Version 2

PF tabular

PF graphical

Supplementary information



		PDS-based	precipitatio	n frequency	estimates v	vith 90% cor	fidence inte	ervals (in inc	:hes)1	
				-	Average recurren	ce interval (years)				
Juration	1	2	5	10	26	50	100	200	500	1000
5-min	0.096 (0.081-0.116)	0.130 (0.109-0.156)	0.180 (0.151-0.217)	0.225 (0.187-0.274)	0.295 (0.236-0.372)	0.355 (0.278-0.458)	9.423 (0.323-0.560)	0.500 (0.370-0.682)	0.618 (0.438-0.881)	0.720 (0.492-1.07
10-min	0.138 (0.116-0.166)	0.186 (0.157-0.224)	0.258 (0.216-0.311)	0,323 (0.268-0.393)	0,423 (0.338-0.533)	0.509 (0.398-0.656)	0,806 (0.463-0.803)	0.717 (0.531-0.978)	0.886 (0.628-1.26)	1.03 (0.706-1.53
15-min	0.167 (0.141-0.201)	0.225 (0.189-0.271)	0.312 (0.261-0.376)	0,380 (0.324-0.475)	0,511 (0.409-0.645)	0.615 (0.482-0.794)	0.738 (0.659-0.971)	0.867 (0.642-1.18)	1.07 (0.759-1.53)	1.25 (0.853-1.85
30-min	0.228 (0.192-0.274)	0.307 (0.258-0.370)	0.425 (0.356-0.513)	0.532 (0.442-0.648)	0,697 (0.558-0.879)	0.840 (0.657-1.08)	1,00 (0.763-1.32)	1.18 (0.876-1.61)	1.46 (1.03-2.08)	1.70 (1.16-2.52)
60-min	0.320 (0.269-0.384)	0.431 (0.362-0.518)	0.596 (0.499-0.719)	0.746 (0.619-0.908)	0.977 (0.782-1.23)	1.18 (0.921-1.52)	1.40 (1.07-1.86)	1.66 (1.23-2.26)	2.05 (1.45-2.92)	2.39 (1.63-3.53)
2-hr	0.426 (0.358-0.512)	0.540 (0.453-0.649)	0.710 (0.594-0.856)	0,865 (0.718-1.05)	1,11 (0.886-1,40)	1.32 (1.03-1.70)	1.56 (1.19-2.06)	1,83 (1.36-2.50)	2.26 (1.60-3.21)	2.63 (1.80-3.88)
3-hr	0.514 (0.432-0.618)	0.637 (0.535-0.766)	0.820 (0.687-0.990)	0.988 (0.820-1.20)	1.25 (1.00-1.58)	1.48 (1.16-1.91)	1.74 (1.33-2.30)	2.04 (1.51-2.78)	2.50 (1.77-3.56)	2.91 (1.99-4.30)
6-hr	0.687 (0.577-0.825)	0.833 (0.699-1.00)	1.05 (0 878-1.26)	1.25 (1.03-1.52)	1.55 (1.24-1.96)	1.82 (1.42-2.34)	2.12 (1.62-2.80)	2.47 (1.83-3.36)	3.01 (2.13-4.28)	3.49 (2.38-5.15
12-hr	0.913 (0.767-1.10)	1.15 (0.964-1.38)	1.48 (1.24-1.79)	1,78 (1.47-2.16)	2.21 (1.77-2.78)	2.57 (2.01-3.31)	2.98 (2.26-3.91)	3,39 (2,51-4.62)	4.01 (2.84-5.72)	4.54
24-hr	1.27 (1.08-1.53)	1.70 (1.45-2.05)	2.30 (1.95-2.77)	2.80 (2.35-3.39)	3.60 (2.87-4.36)	4.07 (3.28-5.15)	4.67 (3.69-6.02)	5.30 (4.10-6.99)	6.20 (4.54-8.45)	6.92 (5.04-9.69)
2-day	1.54 (1.31-1.86)	2.10 (1.78-2.53)	2.88 (2.44-3.47)	3.64 (2.98-4.30)	4.50 (3.69-5.60)	6.28 (4.26-5.68)	6.12 (4.84-7.89)	7.02 (5.44-9.26)	8.32 (6.23-11.3)	9.38 (6.83-13.1)
3-day	1.72 (1.46-2.07)	2.35 (1.99-2.82)	3.25 (2.75-3.91)	4.03 (3.39-4.89)	5.17 (4.24-6.43)	6.11 (4.93-7.73)	7.14 (5.65-9.20)	8.26 (6.39-10.9)	9.90 (7.41-13.5)	11.3 (8.21-15.8)
4-day	1.85 (1.57-2.22)	2.54 (2.15-3.05)	3.53 (2.99-4.25)	4.39 (3.70-5.33)	5.66 (4.64-7.05)	6.72 (5.42-8.50)	7.87 (6.23-10.1)	9.14 (7.07-12.0)	11.0 (8.24-15.0)	12.6 (9.15-17.6)
7-day	2.10 (1.78-2.52)	2.89 (2.45-3.48)	4.04 (3.42-4.87)	5.04 (4.24-6.12)	6.52 (5.35-8.12)	7.75 (6.25-9.81)	9.09 (7.19-11.7)	10.6 (8 17-13.9)	12.7 (9.52-17.3)	14.5 (10.6-20.3)
10-day	2.28 (1.94-2.74)	3.16 (2.68-3.80)	4,42 (3.75-5.33)	5.53 (4.65-6.70)	7.15 (5.86-8.90)	8.49 (6.85-10.7)	9.94 (7.87-12.8)	11.5 (8.92-15.2)	13.9 (10.4-16.9)	15.8 (11.5-22.1
20-day	2,80 (2.38-3,36)	3.93 (3.34-4.73)	5.54 (4.69-6.67)	6.92 (5.83-8.40)	8,93 (7.33-11.1)	10.6 (8.53-13.4)	12.3 (9.74-15.9)	14.2 (11.0-18.7)	16.8 (12.6-23.0)	19.0 (13.8-26.6
30-day	3,30 (2.80-3.96)	4.64 (3.94-5.58)	6.52 (5.53-7.86)	8,14 (6.85-9.87)	10,5 (8,58-13.0)	12.3 (9.95-15.6)	14.3 (11.3-18.4)	16.4 (12.7-21.6)	19.3 (14.4-26.2)	21.6 (15,7-30.2
45-day	3.98 (3.38-4.79)	5.59 (4.74-6.72)	7.81 (6.61-9.41)	9.69 (8.15-11.8)	12.4 (10.1-15.4)	14.5 (11.7-18.3)	16.7 (13.2-21.5)	19.0 (14.7-25.0)	22.1 (16.6-30.2)	24.6 (17.9-34.4
60-day	4.61 (3.92-5.54)	6.42 (5.44-7.71)	8.89 (7.53-10.7)	11.0 (9.23-13.3)	13.9 (11.4-17.3)	16.2 (13.1-20.5)	18.6 (14.7-23.9)	21.0 (16.2-27.7)	24.3 (18.2-33.1)	26.8 (19.5-37.5

Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS)

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information

Estimates from the table in CSV format | Precipitation frequency estimates V | Submit

Figure 3 - Precipitation Frequency Estimates

Existing Flows

SSA was run for both the 10-year and 100-year storms. Refer to Attachment D for the SSA analysis output report for the 10-year storm. Attachment E is the SSA analysis output report for the 100-year storm.

SSA analysis output for the 10-year existing storm indicates a Qex(10) capacity of 297.84 cfs at the point of interest, just south of the proposed road extension. Per Attachment F, Hydraflow Express calculations show that given this capacity, the average velocity of the existing 10-year flow through the existing channel is 6.50 ft/s.

The 100-year storm event was also modelled with the following results: Qex(100) = 602.03 cfs with a maximum velocity of 8.46 ft/s through the existing channel. Attachment F provides the Hydraflow Express calculations for the existing unlined channels for both the 10-year and 100-year flows. These existing flows will be perpetuated with the proposed design.

Proposed Design

The new haul road extension will consist of a 321-lineal foot, 24-foot wide road (2-12-foot lanes with 6-foot shoulders). Within Caltrans right-of-way, the road section will consist of 6 inches of hot-mix asphalt over 1.10 feet of Class 2 aggregate from the US 395 tie-in up to the east extents of the returns. The road section from this point on into Bureau of Land Management (BLM) and private property will consist of 4 inches of hot-mix asphalt over 8 inches of Class 2 aggregate base. Road-section design is shown on the civil plans on both the profile and detail sheets (see sheets P-1 and D-1) provided with this report.

The proposed road and culvert will be designed to concentrate and perpetuate the 10-year storm under and through the road extension. It is proposed that the storm design will include two headwall structures with an entrance (south of the proposed road) and exit (north of the proposed road) with three (3) 48-inch by ~60-foot long corrugated metal pipe (CMP (8-gauge)) culverts.

Attached as Attachment G is a Hydraflow Express culvert report depicting the inlet and outlet conditions and the hydraulic grade lines associated with the new storm design during the 10-year storm. This attachment shows that the proposed storm design will concentrate and perpetuate just over the 10-year storm (at 300 cfs) with a 5.14-foot headwater depth (4728.42 (Hw) -4723.28 (Inlet Invert) = 5.14 feet) with inlet control, which is not anticipated to overtop the new road. The 10-year storm will flow through the new storm structure at no more than 9.80 ft/s.

The maximum capacity of the new storm structure is 474.20 cfs during the 100-year event. Any runoff beyond the maximum capacity of the storm structure (602.03 - 474.20 cfs = 127.83 cfs) is anticipated to overflow atop the low point in the road and head north into the newly aligned channel.

Attachment H is the 100-year Hydraflow Express culvert report showing 474.20 cfs flowing through the new culvert system with the remaining flows (125.80 cfs) overtopping the road. The 100-year storm will flow through the new storm structure at no more than 13.12 ft/s under these conditions.

Runoff flowing upstream and downstream of the proposed storm structure will be perpetuated by trapezoidal channels lined in riprap and graded to a minimum bottom width of 4 feet with 3:1 slopes to a minimum depth of 3 feet. Channeling before and after the new culvert/headwall system will encompass riprap-lined 20-foot bottom widths with 1:5 to 1 side slopes.

Attachment I provides the downstream channel reports for the proposed and improved condition. The affected portions of the channels impacted by this proposed design will be lined with Class V riprap resulting in lower outlet velocities than in the pre-existing condition. The velocities of the downstream channel flows are 5.80 ft/s for the 10-year storm and 6.92 ft/s for the 100-year storm.

Refer to the next section for riprap sizing and depths.

Riprap

Sizing of riprap for the channels was determined by the USACE Modified Maynord et al. Method:

$$D_{30} = (SF)(C_S)(C_V)(C_T)(Y) \left[\sqrt{\frac{\gamma_W}{\gamma_S - \gamma_W}} \times \left(\frac{v}{\sqrt{K_1(g)(d)}}\right) \right]^{2.5}$$

Where:

SF (safety factor) = 1.2

C_s (stability coefficient) = 0.30 for angular rock

 C_V (vertical velocity distribution coefficient) = $1.283 - \log\left(\frac{R}{W}\right) = 1.21$

- Where:
 - o R (centerline radius of bend) = 30 feet
 - o W (water surface width) = 25.6 feet

 C_T (thickness coefficient, from USACOE 1991, EM 1110-2-1601) = 1.0

$$K_1$$
 (side slope correction factor) = $\sqrt{1 - \frac{\sin \Theta}{\sin \Phi}} = 0.713$

- Where:
 - o Θ (angle of side slope [3:1]) = 18.4°
 - Φ (angle of repose) = 40°

Y (depth of water) = 3.54 feet

d (hydraulic depth) \cong 3 feet

 y_W (specific weight of water) = 62.4 pcf

 γ_s (specific weight of stone) = 135 pcf

v (local velocity) = $1.5v_{avg} = 8.70$ fps

• Where: $v_{avg} = 5.80$ fps

g (gravitational acceleration) = 32.2 fps

$$D_{30} = (1.2)(0.30)(1.21)(1.0)(3.54)(0.93)$$

:.
$$D_{30} = 1.44 \ feet \ (17.3 \ inches) \rightarrow \underline{\textbf{Class V riprap}} = 17.0 \ \text{to } 20.5 \ \text{inches} \ (D_{50})$$

 $D_{100} = 36 \ \text{inches}$

T (blanket thickness) = $1.5D_{50}$ or D_{100} = 26 inches or 36 inches whichever is larger.

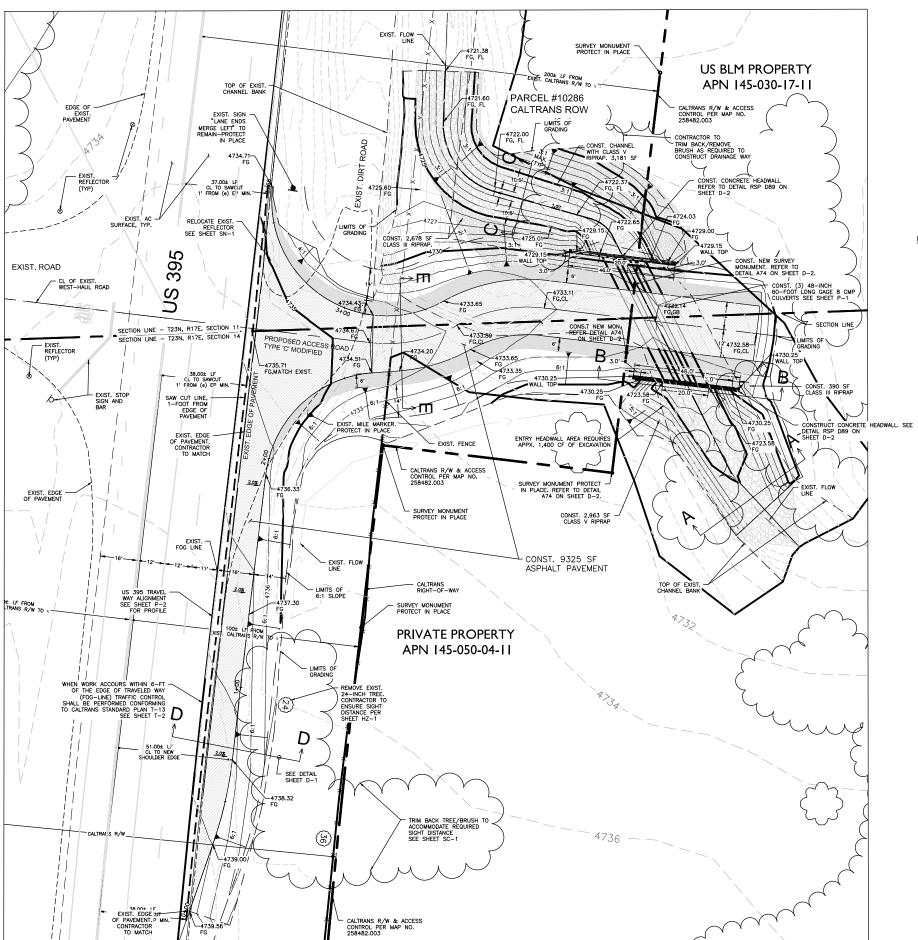
Summit recommends the installation of Class V riprap with a blanket thickness of 36 inches along the channels which will be improved along with the installation of the new culvert system.

Conclusions

The construction of the Geofortis Minerals haul road extension to the eastern side of US 395 will be completed in accordance with Caltrans and AASHTO requirements. The proposed storm facilities will encompass 2 headwalls (entrance and exit) incorporating three 60-foot long 48-inch CMP barrels which will concentrate and perpetuate the 10-year storm. The capacity of this structure will allow as much as 474.20 cfs of storm waters without overtopping the road extension.

The 100-year storm is anticipated to produce as much as 602.03 cfs where the proposed storm structure will allow as much as 410 cfs without overtopping the road. During the 100-year event, it is anticipated that approximately 125.80 cfs (with 474.20 cfs through the culvert storm structure) will overtop the road and flow northerly along trapezoidal channels graded to 4 feet in bottom width with 3:1 slopes at a minimum depth of 3 feet. The channels will be lined with a minimum 36-inch thick blanket of Class V riprap.

Attachment A PROJECT SITE MAPPING





RIP RAP AC PAVEMENT

ROAD SHOULDER

EXIST. FLOW LINE

PROPOSED FLOW LINE

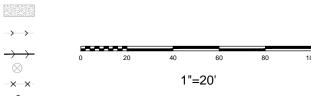
EXIST. DELINEATOR

EXIST. FENCE EXIST. SIGN 0

TIE IN POINT

SURVEY MONUMENT NEW DELINEATOR

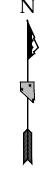
PROPOSED SIGN



NOTES:

- 1. CONTRACTOR TO TRIM AND/OR REMOVE TREES/BUSHES WITHIN THE SIGHT TRIANGLES SHOWN ON SHEET S-1 AS REQUIRED TO CONSTRUCT IMPROVEMENTS.

 2. WHEN WORK OCCURS WITHIN 6-FEET OF THE EDGE OF TRAVELLED WAY (FOG-LINE), TRAFFIC
- CONTROL SHALL BE PERFORMED CONFORMING TO CALTRANS STANDARD PLAN T-13 SHOWN ON SHEET D-1 (AND TC-1 OF THESE PLANS). CONTRACTOR SHALL PROVIDE AT LEAST ONE PERSON TO CONTINUOUSLY MAINTAIN TRAFFIC CONTROL DEVICES FOR LANE CLOSURES DURING CONSTRUCTION.
 3. FOR SIGNAGE AND POST RELOCATION, SEE SHEET SN-1



CUT/FILL VOLUMES

CUT = 500 CY FILL = 2000 CY NET ADJUSTED = 1500 CY

RIP RAP OUANTITIES

CLASS III RIPRAP 3,068 SF **CLASS V RIPRAP** 6,144 SF



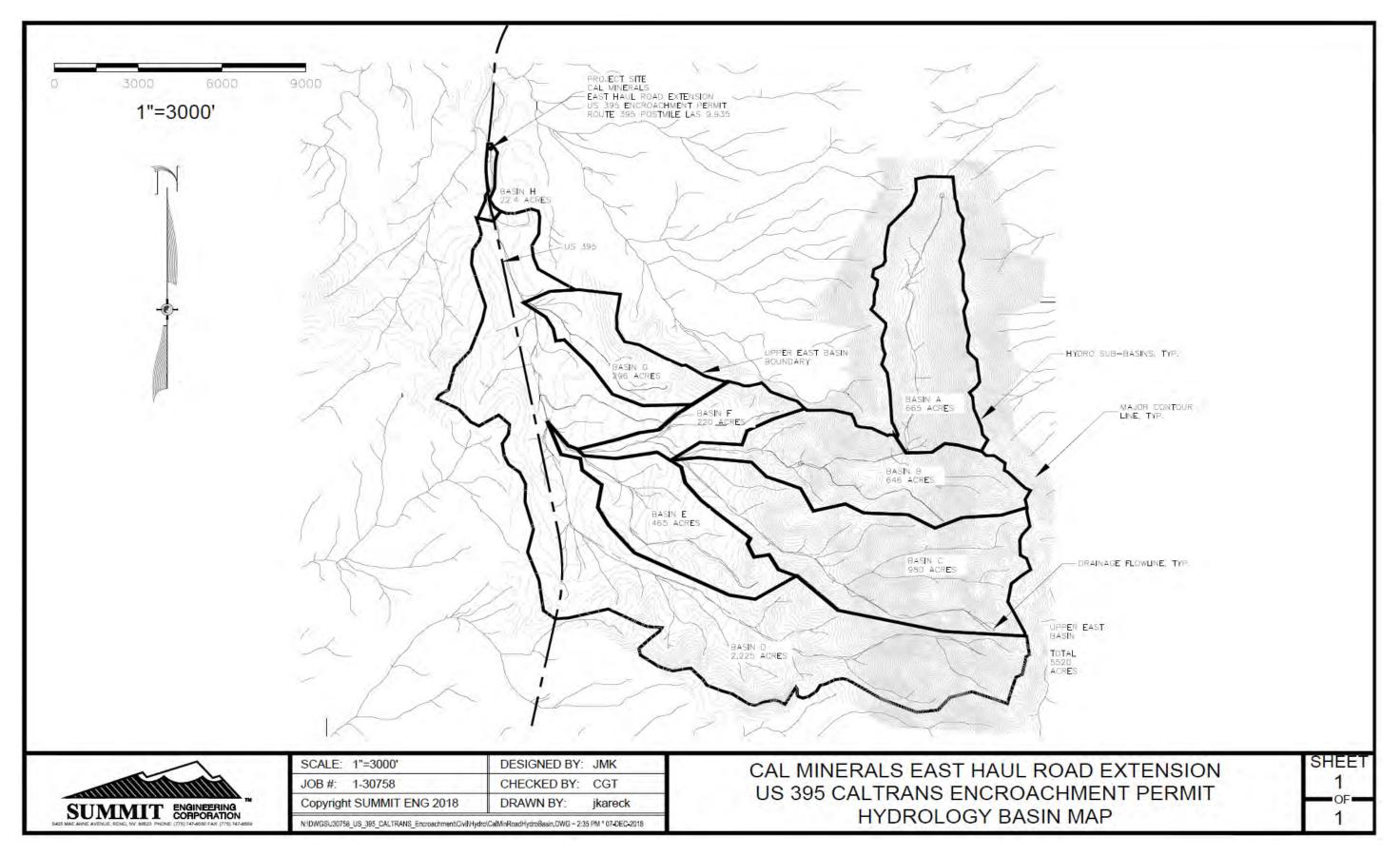


DESIGNED BY	DRAWN BY:	CHECKED BY:	
LS. LLC	AT PERMIT	Z	•

GEOFORTIS MINERAL: US 395 ENCROACHMENT GRADING PLAN

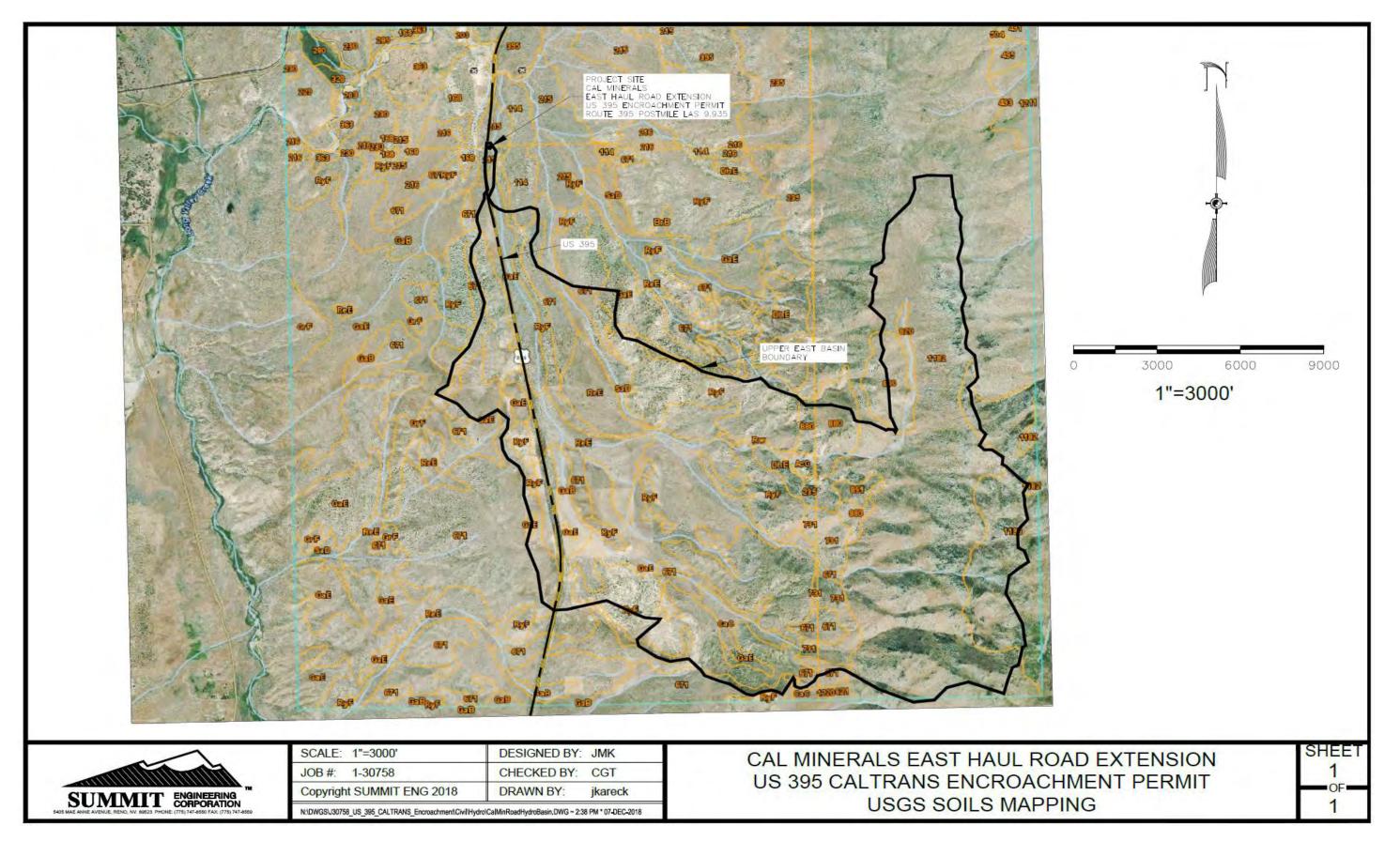
SHEET **G-1** 10

Attachment B EXISTING HYDROLOGY BASIN MAPPING



Attachment C

USGS SOILS MAPPING



Attachment D

SSA Analysis Results

10-YR Existing Storm Report

Project Description

File Name CAL-MINERALS_EX-10-YR.SPF

Project Options

Flow Units	CFS
Elevation Type	Elevation
Hydrology Method	Rational
Time of Concentration (TOC) Method	Kirpich
Link Routing Method	Kinematic Wave
Enable Overflow Ponding at Nodes	YES
Skip Steady State Analysis Time Periods	NO

Analysis Options

Start Analysis On	Oct 26, 2018	00:00:00
End Analysis On	Oct 27, 2018	00:00:00
Start Reporting On	Oct 26, 2018	00:00:00
Antecedent Dry Days	0	days
Runoff (Dry Weather) Time Step	0 01:00:00	days hh:mm:ss
Runoff (Wet Weather) Time Step	0 00:05:00	days hh:mm:ss
Reporting Time Step	0 00:05:00	days hh:mm:ss
Routing Time Step	30	seconds

Number of Elements

	Qt
Rain Gages	0
Subbasins	5
Nodes	9
Junctions	
Outfalls	0
Flow Diversions	0
Inlets	0
Storage Nodes	0
Links	8
Channels	8
Pipes	0
Pumps	0
Orifices	0
Weirs	0
Outlets	0
Pollutants	0
Land Uses	0

Rainfall Details

Subbasin Summary

SN Subbasin ID	Area	Weighted Runoff	Average Slope	Flow Length	Total Rainfall	Total Runoff	Total Runoff	Peak Runoff	Time of Concentration
		Coefficient					Volume		
	(ac)		(%)	(ft)	(in)	(in)	(ac-in)	(cfs)	(days hh:mm:ss)
1 Sub-01	665.00	0.3700	50.0000	10270.00	0.08	0.03	18.62	88.16	0 00:12:30
2 Sub-02	1646.00	0.3700	35.0000	13800.00	0.13	0.05	77.36	257.73	0 00:18:00
3 Sub-05	465.00	0.3700	30.0000	6455.00	0.06	0.02	10.23	57.20	0 00:10:38
4 Sub-06	2225.00	0.3700	25.0000	20628.00	0.24	0.09	198.03	424.10	0 00:27:55
5 Sub-07	22.40	0.3700	15.0000	2594.00	0.05	0.02	0.45	2.68	0 00:10:00

Node Summary

CNI Flament	Class 2.24	1	O 1/D:	1-141-1	C	Dandad	Daal.	Mandage		N 4:	T: f	T-4-1	Tatal Time
SN Element	Element		Ground/Rim		Surcharge			Max HGL	Max	Min	Time of		Total Time
ID	Type	Elevation	(Max)	Water	Elevation	Area	Inflow	Elevation	Surcharge	Freeboard	Peak	Flooded	Flooded
			Elevation	Elevation				Attained	Depth	Attained	Flooding	Volume	
									Attained		Occurrence		
		(ft)	(ft)	(ft)	(ft)	(ft ²)	(cfs)	(ft)	(ft)	(ft)	(days hh:mm)	(ac-in)	(min)
1 Jun-05	Junction	5935.00	100.00	0.00	0.00	0.00	14.24	5936.45	0.00	798.55	0 00:00	0.00	0.00
2 Jun-06	Junction	5490.00	100.00	0.00	0.00	0.00	0.00	5490.00	0.00	800.00	0 00:00	0.00	0.00
3 Jun-07	Junction	5006.00	100.00	0.00	0.00	0.00	257.73	5007.29	0.00	398.71	0 00:00	0.00	0.00
4 Jun-08	Junction	4938.00	100.00	0.00	0.00	0.00	222.97	4939.06	0.00	398.94	0 00:00	0.00	0.00
5 Jun-09	Junction	4888.00	100.00	0.00	0.00	0.00	620.56	4890.27	0.00	297.73	0 00:00	0.00	0.00
6 Jun-10	Junction	4840.00	100.00	0.00	0.00	0.00	548.10	4852.47	0.00	287.53	0 00:00	0.00	0.00
7 Jun-11	Junction	4840.00	50.00	0.00	0.00	0.00	312.39	4848.95	0.00	41.05	0 00:00	0.00	0.00
8 Out-03	Junction	4730.00	50.00	0.00	0.00	0.00	297.84	4734.00	0.00	0.00	0 00:00	0.00	0.00
9 UpperEastBasin	Junction	6694.00	100.00	0.00	0.00	0.00	88.16	6694.10	0.00	199.90	0 00:00	0.00	0.00

Link Summary

SN Element ID	Element Type	From (Inlet)	To (Outlet) Node	Length	Inlet Invert	Outlet Invert	0	Diameter or Height	Manning's Roughness	Peak Flow	Design Flow Capacity	Peak Flow/ Design Flow		Peak Flow Depth		Total Time Reported Surcharged Condition
		Node			Elevation	Elevation						Ratio			Total Depth	
															Ratio	
				(ft)	(ft)	(ft)	(%)	(in)		(cfs)	(cfs)		(ft/sec)	(ft)		(min)
1 Link-03	Channel	UpperEastBasin	Jun-05	10270.00	6694.00	5935.00	7.3900	2400.000	0.0400	14.24	40096768.26	0.00	0.72	0.05	0.00	0.00
2 Link-04	Channel	Jun-05	Jun-06	4132.00	5935.00	5490.00	10.7700	9600.000	0.0400	0.00	813440873.53	0.00	0.00	0.73	0.00	0.00
3 Link-05	Channel	Jun-06	Jun-07	4753.00	5490.00	5006.00	10.1800	2700.000	0.0400	0.00	43773442.64	0.00	0.00	0.00	0.00	0.00
4 Link-06	Channel	Jun-07	Jun-08	3804.00	5006.00	4938.00	1.7900	4800.000	0.0400	222.97	82279903.09	0.00	9.74	1.06	0.00	0.00
5 Link-07	Channel	Jun-08	Jun-09	1770.00	4938.00	4888.00	2.8200	3600.000	0.0400	273.90	48722679.32	0.00	12.65	0.89	0.00	0.00
6 Link-08	Channel	Jun-09	Jun-10	4753.00	4888.00	4840.00	1.0100	3600.000	0.0400	548.10	29131946.60	0.00	9.48	2.05	0.01	0.00
7 Link-09	Channel	Jun-10	Jun-11	3500.00	4840.00	4840.00	0.0000	600.000	0.0400	312.39	6215.06	0.05	0.17	6.39	0.13	0.00
8 Link-10	Channel	Jun-11	Out-03	2594.00	4840.00	4730.00	4.2400	48.000	0.0400	297.84	19546.55	0.02	3.64	0.33	0.08	0.00

Subbasin Hydrology

Subbasin: Sub-01

Input Data

Area (ac)	665.00
Weighted Runoff Coefficient	0.3700
Average Slope (%)	50.0000
Flow Length (ft)	10270.00

Runoff Coefficient

on occinoione			
	Area	Soil	Runoff
Soil/Surface Description	(acres)	Group	Coeff.
Pasture, 25 years or greater	665.00	A (6%+)	0.37
Composite Area & Weighted Runoff Coeff.	665.00		0.37

Time of Concentration

TOC Method : Kirpich

Sheet Flow Equation :

Tc = (0.0078 * ((Lf^0.77) * (Sf^-0.385)))

Where:

Tc = Time of Concentration (min) Lf = Flow Length (ft) Sf = Slope (ft/ft)

 Flow Length (ft)
 10270.00

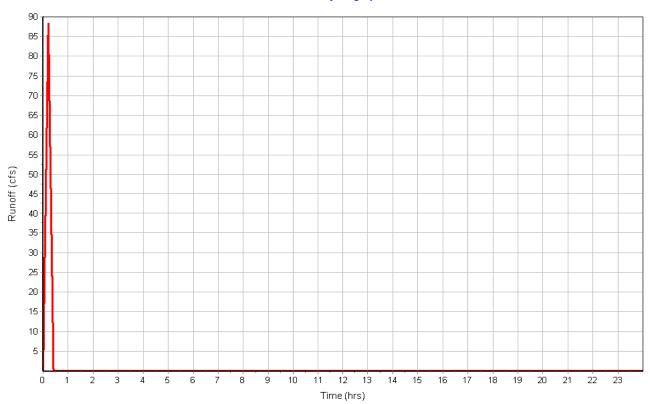
 Slope (%)
 50

 Computed TOC (min)
 12.50

Subbasin Runoff Results

Total Rainfall (in)	0.08
Total Runoff (in)	0.03
Peak Runoff (cfs)	88.16
Rainfall Intensity	0.358
Weighted Runoff Coefficient	0.3700
Time of Concentration (days hh:mm:ss)	0 00:12:30

Runoff Hydrograph



Input Data

Area (ac)	1646.00
Weighted Runoff Coefficient	0.3700
Average Slope (%)	35.0000
Flow Length (ft)	13800.00

Runoff Coefficient

"	on Coemcient			
		Area	Soil	Runoff
	Soil/Surface Description	(acres)	Group	Coeff.
	Pasture, 25 years or greater	1646.00	A (6%+)	0.37
	Composite Area & Weighted Runoff Coeff.	1646.00		0.37
	Composito / troa a 11 orgintoa i tarioni Coom.	. 5 10.00		3.01

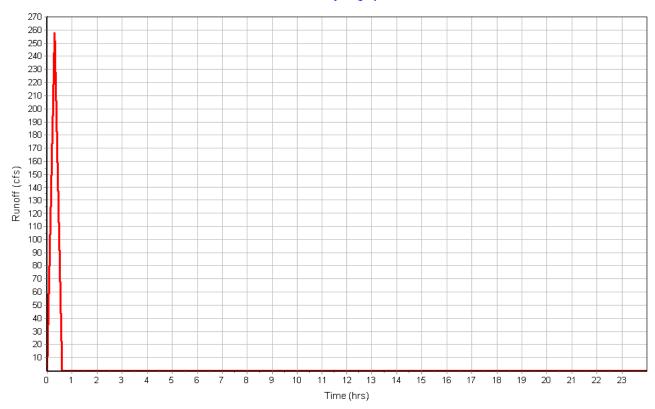
Time of Concentration

Flow Length (ft)	13800.00
Slope (%)	35
Computed TOC (min)	18.00

Subbasin Runoff Results

Total Rainfall (in)	0.13
Total Runoff (in)	0.05
Peak Runoff (cfs)	257.73
Rainfall Intensity	0.423
Weighted Runoff Coefficient	0.3700
Time of Concentration (days hh:mm:ss)	0 00:18:00

Runoff Hydrograph



Input Data

Area (ac)	465.00
Weighted Runoff Coefficient	0.3700
Average Slope (%)	30.0000
Flow Length (ft)	6455.00

Runoff Coefficient

Runott
Coeff.
0.37
0.37
0.

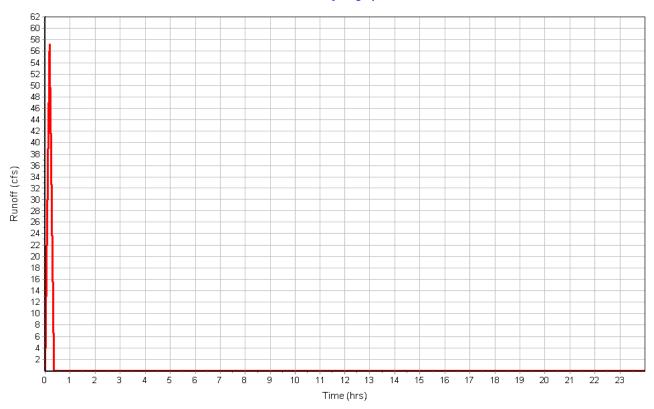
Time of Concentration

Flow Length (ft)	6455.00
Slope (%)	30
Computed TOC (min)	10.64

Subbasin Runoff Results

Total Rainfall (in)	0.06
Total Runoff (in)	0.02
Peak Runoff (cfs)	57.20
Rainfall Intensity	0.332
Weighted Runoff Coefficient	0.3700
Time of Concentration (days hh:mm:ss)	0 00:10:38

Runoff Hydrograph



Input Data

Area (ac)	2225.00
Weighted Runoff Coefficient	0.3700
Average Slope (%)	25.0000
Flow Length (ft)	20628.00

Runoff Coefficient

	Area	Soli	Runorr
Soil/Surface Description	(acres)	Group	Coeff.
Pasture, 25 years or greater	2225.00	A (6%+)	0.37
Composite Area & Weighted Runoff Coeff.	2225.00		0.37

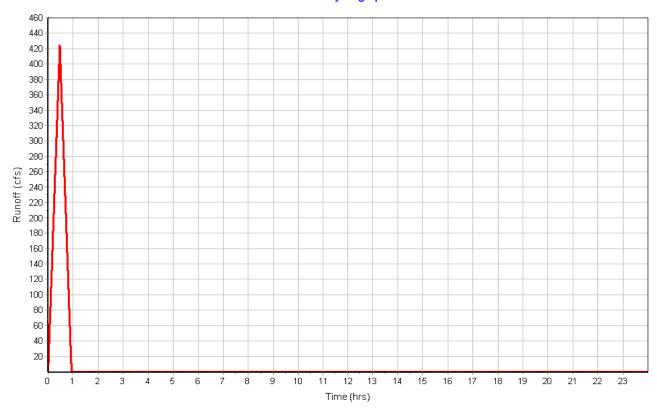
Time of Concentration

Flow Length (ft)	20628.00
Slope (%)	25
Computed TOC (min)	27.92

Subbasin Runoff Results

Total Rainfall (in)	0.24
Total Runoff (in)	0.09
Peak Runoff (cfs)	424.10
Rainfall Intensity	0.515
Weighted Runoff Coefficient	0.3700
Time of Concentration (days hh:mm:ss)	0 00:27:55

Runoff Hydrograph



Input Data

Area (ac)	22.40
Weighted Runoff Coefficient	
Average Slope (%)	15.0000
Flow Length (ft)	2594 00

Runoff Coefficient

	Area	5011	Runott
Soil/Surface Description	(acres)	Group	Coeff.
Pasture, 25 years or greater	22.40	A (6%+)	0.37
Composite Area & Weighted Runoff Coeff.	22.40		0.37

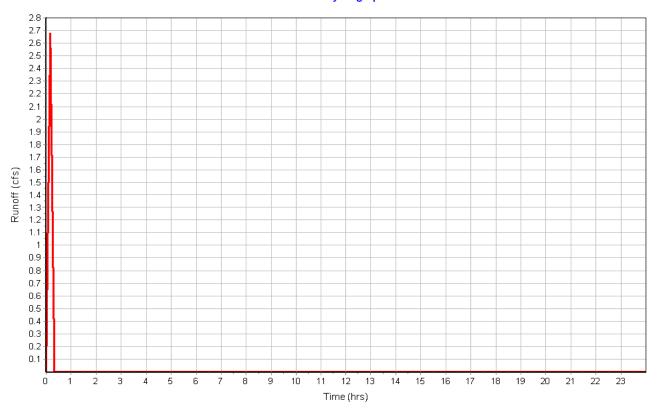
Time of Concentration

Flow Length (ft)	2594.00
Slope (%)	15
Computed TOC (min)	6.89

Subbasin Runoff Results

Total Rainfall (in)	0.05
Total Runoff (in)	0.02
Peak Runoff (cfs)	2.68
Rainfall Intensity	0.323
Weighted Runoff Coefficient	0.3700
Time of Concentration (days hh:mm:ss)	0 00:06:53

Runoff Hydrograph



Junction Input

SN Element	Invert	Ground/Rim	Ground/Rim	Initial	Initial	Surcharge	Surcharge	Ponded	Minimum
ID	Elevation	(Max)	(Max)	Water	Water	Elevation	Depth	Area	Pipe
		Elevation	Offset	Elevation	Depth				Cover
	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft ²)	(in)
1 Jun-05	5935.00	100.00	-5835.00	0.00	-5935.00	0.00	-100.00	0.00	0.00
2 Jun-06	5490.00	100.00	-5390.00	0.00	-5490.00	0.00	-100.00	0.00	0.00
3 Jun-07	5006.00	100.00	-4906.00	0.00	-5006.00	0.00	-100.00	0.00	0.00
4 Jun-08	4938.00	100.00	-4838.00	0.00	-4938.00	0.00	-100.00	0.00	0.00
5 Jun-09	4888.00	100.00	-4788.00	0.00	-4888.00	0.00	-100.00	0.00	0.00
6 Jun-10	4840.00	100.00	-4740.00	0.00	-4840.00	0.00	-100.00	0.00	0.00
7 Jun-11	4840.00	50.00	-4790.00	0.00	-4840.00	0.00	-50.00	0.00	0.00
8 Out-03	4730.00	50.00	-4680.00	0.00	-4730.00	0.00	-50.00	0.00	0.00
9 UpperEastBasin	6694.00	100.00	-6594.00	0.00	-6694.00	0.00	-100.00	0.00	0.00

Junction Results

SN Element	Peak	Peak	Max HGL	Max HGL	Max	Min	Average HGL	Average HGL	Time of	Time of	Total	Total Time
ID	Inflow	Lateral	Elevation	Depth	Surcharge	Freeboard	Elevation	Depth	Max HGL	Peak	Flooded	Flooded
		Inflow	Attained	Attained	Depth	Attained	Attained	Attained	Occurrence	Flooding	Volume	
					Attained					Occurrence		
	(cfs)	(cfs)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(days hh:mm)	(days hh:mm)	(ac-in)	(min)
1 Jun-05	14.24	0.00	5936.45	1.45	0.00	798.55	5935.01	0.01	0 00:19	0 00:00	0.00	0.00
2 Jun-06	0.00	0.00	5490.00	0.00	0.00	800.00	5490.00	0.00	0 00:00	0 00:00	0.00	0.00
3 Jun-07	257.73	257.73	5007.29	1.29	0.00	398.71	5006.02	0.02	0 00:18	0 00:00	0.00	0.00
4 Jun-08	222.97	57.20	4939.06	1.06	0.00	398.94	4938.02	0.02	0 00:31	0 00:00	0.00	0.00
5 Jun-09	620.56	424.10	4890.27	2.27	0.00	297.73	4888.05	0.05	0 00:28	0 00:00	0.00	0.00
6 Jun-10	548.10	0.00	4852.47	12.47	0.00	287.53	4840.34	0.34	0 00:36	0 00:00	0.00	0.00
7 Jun-11	312.39	2.68	4848.95	8.95	0.00	41.05	4843.63	3.63	0 01:20	0 00:00	0.00	0.00
8 Out-03	297.84	0.00	4734.00	4.00	0.00	0.00	4733.96	3.96	0 00:10	0 00:00	0.00	0.00
9 UpperEastBasin	88.16	88.16	6694.10	0.10	0.00	199.90	6694.00	0.00	0 00:12	0 00:00	0.00	0.00

Channel Input

SN Element ID	Length	Inlet Invert		Outlet Invert	Outlet Invert		Average Slope		Height	Width	Manning's Roughness	Entrance Losses	Exit/Bend Losses		Initial Flap Flow Gate
		Elevation	Offset	Elevation	Offset										
	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(%)		(ft)	(ft)					(cfs)
1 Link-03	10270.00	6694.00	0.00	5935.00	0.00	759.00	7.3900	Trapezoidal	200.000	1200.000	0.0400	0.5000	0.5000	0.0000	0.00 No
2 Link-04	4132.00	5935.00	0.00	5490.00	0.00	445.00	10.7700	Trapezoidal	800.000	3240.000	0.0400	0.5000	0.5000	0.0000	0.00 No
3 Link-05	4753.00	5490.00	0.00	5006.00	0.00	484.00	10.1800	Trapezoidal	225.000	1390.000	0.0400	0.5000	0.5000	0.0000	0.00 No
4 Link-06	3804.00	5006.00	0.00	4938.00	0.00	68.00	1.7900	Trapezoidal	400.000	2440.000	0.0400	0.5000	0.5000	0.0000	0.00 No
5 Link-07	1770.00	4938.00	0.00	4888.00	0.00	50.00	2.8200	Trapezoidal	300.000	1840.000	0.0400	0.5000	0.5000	0.0000	0.00 No
6 Link-08	4753.00	4888.00	0.00	4840.00	0.00	48.00	1.0100	Trapezoidal	300.000	1840.000	0.0400	0.5000	0.5000	0.0000	0.00 No
7 Link-09	3500.00	4840.00	0.00	4840.00	0.00	0.00	0.0000	Trapezoidal	50.000	700.000	0.0400	0.5000	0.5000	0.0000	0.00 No
8 Link-10	2594 00	4840 00	0.00	4730 00	0.00	110 00	4 2400	Trapezoidal	4 000	274 000	0.0400	0.5000	0.5000	0.0000	0.00 No

Channel Results

SN Element ID	Peak Flow	Time of Peak Flow		Peak Flow/ Design Flow	Peak Flow Velocity	Travel Time	Peak Flow Depth			Froude Reported Number Condition
		Occurrence		Ratio				Total Depth		
								Ratio		
	(cfs)	(days hh:mm)	(cfs)		(ft/sec)	(min)	(ft)		(min)	
1 Link-03	14.24	0 00:19	40096768.26	0.00	0.72	237.73	0.05	0.00	0.00	
2 Link-04	0.00	0 00:00	813440873.53	0.00	0.00		0.73	0.00	0.00	
3 Link-05	0.00	0 00:00	43773442.64	0.00	0.00		0.00	0.00	0.00	
4 Link-06	222.97	0 00:31	82279903.09	0.00	9.74	6.51	1.06	0.00	0.00	
5 Link-07	273.90	0 00:41	48722679.32	0.00	12.65	2.33	0.89	0.00	0.00	
6 Link-08	548.10	0 00:36	29131946.60	0.00	9.48	8.36	2.05	0.01	0.00	
7 Link-09	312.39	0 01:20	6215.06	0.05	0.17	343.14	6.39	0.13	0.00	
8 Link-10	297.84	0 01:36	19546.55	0.02	3.64	11.88	0.33	0.08	0.00	

Attachment E

SSA Analysis Results

100-YR Existing Storm Report

Project Description

Project Options

Flow Units	CFS
Elevation Type	Elevation
Hydrology Method	Rational
Time of Concentration (TOC) Method	Kirpich
Link Routing Method	Kinematic Wave
Enable Overflow Ponding at Nodes	YES
Skip Steady State Analysis Time Periods	NO

Analysis Options

Start Analysis On	Oct 26, 2018	00:00:00
End Analysis On	Oct 27, 2018	00:00:00
Start Reporting On	Oct 26, 2018	00:00:00
Antecedent Dry Days	0	days
Runoff (Dry Weather) Time Step	0 01:00:00	days hh:mm:ss
Runoff (Wet Weather) Time Step	0 00:05:00	days hh:mm:ss
Reporting Time Step	0 00:05:00	days hh:mm:ss
Routing Time Step	30	seconds

Number of Elements

	Qty
Rain Gages	0
Subbasins	5
Nodes	
Junctions	
Outfalls	0
Flow Diversions	0
Inlets	0
Storage Nodes	0
Links	8
Channels	8
Pipes	0
Pumps	0
Orifices	0
Weirs	0
Outlets	0
Pollutants	0
Land Uses	0

Rainfall Details

Subbasin Summary

SN Subbasin ID	Area	Weighted Runoff	Average Slope	Flow Length	Total Rainfall	Total Runoff	Total Runoff	Peak Runoff	Time of Concentration
		Coefficient					Volume		
	(ac)		(%)	(ft)	(in)	(in)	(ac-in)	(cfs)	(days hh:mm:ss)
1 Sub-01	665.00	0.3700	50.0000	10270.00	0.14	0.05	34.58	165.57	0 00:12:30
2 Sub-02	1646.00	0.3700	35.0000	13800.00	0.24	0.09	144.85	484.42	0 00:18:00
3 Sub-05	465.00	0.3700	30.0000	6455.00	0.11	0.04	19.07	107.34	0 00:10:38
4 Sub-06	2225.00	0.3700	25.0000	20628.00	0.45	0.17	371.58	797.16	0 00:27:55
5 Sub-07	22.40	0.3700	15.0000	2594.00	0.10	0.04	0.83	5.02	0 00:10:00

Node Summary

SN Element ID	Element Type	Invert Elevation	Ground/Rim (Max)	Initial Water	Surcharge Elevation	Ponded Area	Peak Inflow	Max HGL Elevation	Max Surcharge	Min Freeboard	Time of Peak	Total Flooded	Total Time Flooded
.5	. , po	2.0740	, ,	Elevation	2.0140	700		Attained	Depth	Attained	Flooding		1 100000
									Attained		Occurrence		
		(ft)	(ft)	(ft)	(ft)	(ft ²)	(cfs)	(ft)	(ft)	(ft)	(days hh:mm)	(ac-in)	(min)
1 Jun-05	Junction	5935.00	100.00	0.00	0.00	0.00	107.74	5936.52	0.00	798.48	0 00:00	0.00	0.00
2 Jun-06	Junction	5490.00	100.00	0.00	0.00	0.00	0.00	5490.00	0.00	800.00	0 00:00	0.00	0.00
3 Jun-07	Junction	5006.00	100.00	0.00	0.00	0.00	484.42	5007.73	0.00	398.27	0 00:00	0.00	0.00
4 Jun-08	Junction	4938.00	100.00	0.00	0.00	0.00	407.46	4939.51	0.00	398.49	0 00:00	0.00	0.00
5 Jun-09	Junction	4888.00	100.00	0.00	0.00	0.00	1188.80	4891.29	0.00	296.71	0 00:00	0.00	0.00
6 Jun-10	Junction	4840.00	100.00	0.00	0.00	0.00	1103.02	4858.77	0.00	281.23	0 00:00	0.00	0.00
7 Jun-11	Junction	4840.00	50.00	0.00	0.00	0.00	624.44	4853.46	0.00	36.54	0 00:00	0.00	0.00
8 Out-03	Junction	4730.00	50.00	0.00	0.00	0.00	602.03	4733.00	0.00	0.00	0 00:00	0.00	0.00
9 UpperEastBasin	Junction	6694.00	100.00	0.00	0.00	0.00	165.57	6694.15	0.00	199.85	0 00:00	0.00	0.00

Link Summary

SN Element ID	Element Type	From (Inlet)	To (Outlet) Node	Length	Inlet Invert	Outlet Invert	Average Slope	Diameter or Height	Manning's Roughness	Peak Flow	•	Peak Flow/ Design Flow	Peak Flow Velocity	Peak Flow Depth		Total Time Reported Surcharged Condition
		Node			Elevation	Elevation		_	-			Ratio	-		Total Depth	_
															Ratio	
				(ft)	(ft)	(ft)	(%)	(in)		(cfs)	(cfs)		(ft/sec)	(ft)		(min)
1 Link-03	Channel	UpperEastBasin	Jun-05	10270.00	6694.00	5935.00	7.3900	2400.000	0.0400	107.74	40096768.26	0.00	4.74	0.08	0.00	0.00
2 Link-04	Channel	Jun-05	Jun-06	4132.00	5935.00	5490.00	10.7700	9600.000	0.0400	0.00	813440873.53	0.00	0.00	0.76	0.00	0.00
3 Link-05	Channel	Jun-06	Jun-07	4753.00	5490.00	5006.00	10.1800	2700.000	0.0400	0.00	43773442.64	0.00	0.00	0.00	0.00	0.00
4 Link-06	Channel	Jun-07	Jun-08	3804.00	5006.00	4938.00	1.7900	4800.000	0.0400	407.46	82279903.09	0.00	11.54	1.52	0.00	0.00
5 Link-07	Channel	Jun-08	Jun-09	1770.00	4938.00	4888.00	2.8200	3600.000	0.0400	401.30	48722679.32	0.00	12.84	1.32	0.00	0.00
6 Link-08	Channel	Jun-09	Jun-10	4753.00	4888.00	4840.00	1.0100	3600.000	0.0400	1103.02	29131946.60	0.00	11.21	3.06	0.01	0.00
7 Link-09	Channel	Jun-10	Jun-11	3500.00	4840.00	4840.00	0.0000	600.000	0.0400	624.44	6215.06	0.10	0.22	9.53	0.19	0.00
8 Link-10	Channel	Jun-11	Out-03	2594.00	4840.00	4730.00	4.2400	36.000	0.0400	602.03	12056.80	0.05	4.81	0.50	0.17	0.00

Subbasin Hydrology

Subbasin: Sub-01

Input Data

Area (ac)	665.00
Weighted Runoff Coefficient	0.3700
Average Slope (%)	50.0000
Flow Length (ft)	10270.00

Runoff Coefficient

Area	2011	Runon
(acres)	Group	Coeff.
665.00	A (6%+)	0.37
665.00		0.37
	(acres) 665.00	(acres) Group 665.00 A (6%+)

Time of Concentration

TOC Method : Kirpich

Sheet Flow Equation :

Tc = (0.0078 * ((Lf^0.77) * (Sf^-0.385)))

Where:

Tc = Time of Concentration (min) Lf = Flow Length (ft)

Sf = Slope (ft/ft)

 Flow Length (ft)
 10270.00

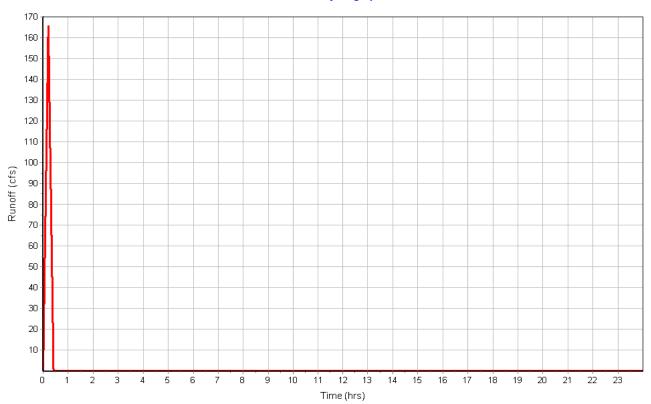
 Slope (%)
 50

 Computed TOC (min)
 12.50

Subbasin Runoff Results

Total Rainfall (in)	0.14
Total Runoff (in)	0.05
Peak Runoff (cfs)	165.57
Rainfall Intensity	0.673
Weighted Runoff Coefficient	0.3700
Time of Concentration (days hh:mm:ss)	0 00:12:30

Runoff Hydrograph



Input Data

Area (ac)	1646.00
Weighted Runoff Coefficient	0.3700
Average Slope (%)	35.0000
Flow Length (ft)	13800.00

Runoff Coefficient

	Area	Soli	Runott
Soil/Surface Description	(acres)	Group	Coeff.
Pasture, 25 years or greater	1646.00	A (6%+)	0.37
Composite Area & Weighted Runoff Coeff.	1646.00		0.37
Composite Area & Weighted Ruhon Coen.	10-0.00		0.01

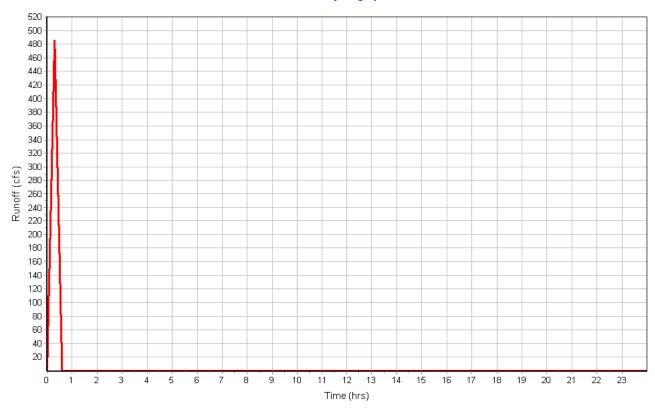
Time of Concentration

Flow Length (ft)	13800.00
Slope (%)	35
Computed TOC (min)	18.00

Subbasin Runoff Results

Total Rainfall (in)	0.24
Total Runoff (in)	0.09
Peak Runoff (cfs)	484.42
Rainfall Intensity	0.795
Weighted Runoff Coefficient	0.3700
Time of Concentration (days hh:mm:ss)	0 00:18:00

Runoff Hydrograph



Input Data

Area (ac)	465.00
Weighted Runoff Coefficient	0.3700
Average Slope (%)	30.0000
Flow Length (ft)	6455.00

Runoff Coefficient

Area	Soli	Runott
(acres)	Group	Coeff.
465.00	A (6%+)	0.37
465.00		0.37
	(acres) 465.00	(acres) Group 465.00 A (6%+)

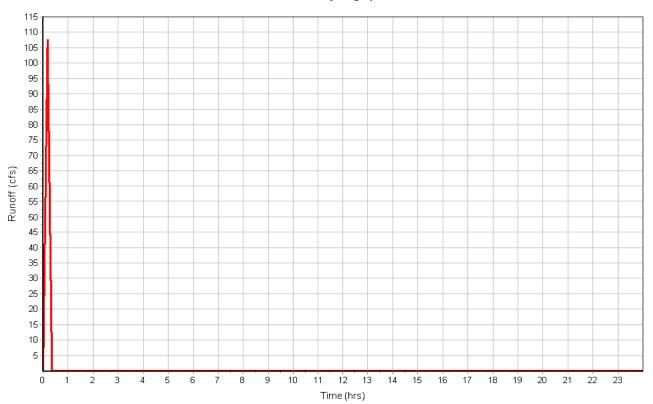
Time of Concentration

Flow Length (ft)	6455.00
Slope (%)	30
Computed TOC (min)	10.64

Subbasin Runoff Results

Total Rainfall (in)	0.11
Total Runoff (in)	0.04
Peak Runoff (cfs)	107.34
Rainfall Intensity	0.624
Weighted Runoff Coefficient	0.3700
Time of Concentration (days hh:mm:ss)	0 00:10:38

Runoff Hydrograph



Input Data

Area (ac)	2225.00
Weighted Runoff Coefficient	0.3700
Average Slope (%)	25.0000
Flow Length (ft)	20628.00

Runoff Coefficient

Area	Soll	Runorr
acres)	Group	Coeff.
25.00 A	(6%+)	0.37
25.00		0.37
	acres) 25.00 A	acres) Group 25.00 A (6%+)

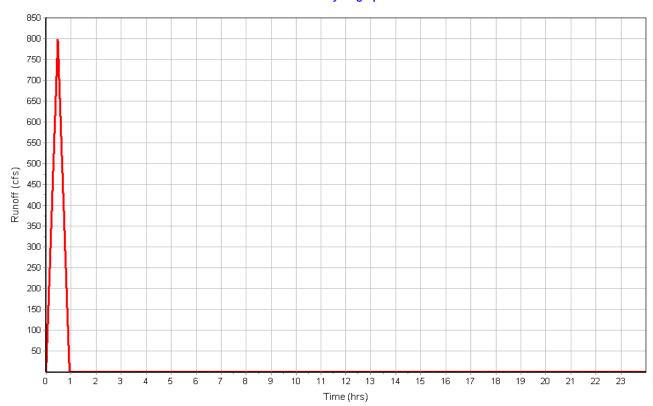
Time of Concentration

Flow Length (ft)	20628.00
Slope (%)	25
Computed TOC (min)	27.92

Subbasin Runoff Results

Total Rainfall (in)	0.45
Total Runoff (in)	0.17
Peak Runoff (cfs)	797.16
Rainfall Intensity	0.968
Weighted Runoff Coefficient	0.3700
Time of Concentration (days hh:mm:ss)	0 00:27:55

Runoff Hydrograph



Input Data

Area (ac)	22.40
Weighted Runoff Coefficient	0.3700
Average Slope (%)	15.0000
Flow Length (ft)	2594.00

Runoff Coefficient

	Area	Soil	Runoff
Soil/Surface Description	(acres)	Group	Coeff.
Pasture, 25 years or greater	22.40	A (6%+)	0.37
Composite Area & Weighted Runoff Coeff.	22.40		0.37

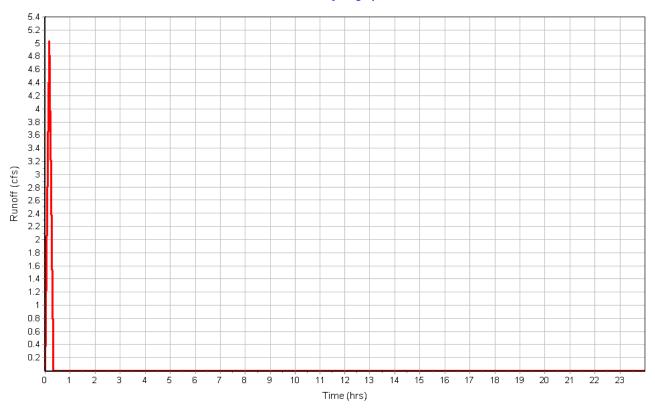
Time of Concentration

Flow Length (ft)	2594.00
Slope (%)	15
Computed TOC (min)	6.89

Subbasin Runoff Results

Total Rainfall (in)	0.10
Total Runoff (in)	0.04
Peak Runoff (cfs)	5.02
Rainfall Intensity	0.606
Weighted Runoff Coefficient	0.3700
Time of Concentration (days hh:mm:ss)	0 00:06:53

Runoff Hydrograph



Junction Input

SN Element	Invert	Ground/Rim	Ground/Rim	Initial	Initial	Surcharge	Surcharge	Ponded	Minimum
ID	Elevation	(Max)	(Max)	Water	Water	Elevation	Depth	Area	Pipe
		Elevation	Offset	Elevation	Depth				Cover
	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft ²)	(in)
1 Jun-05	5935.00	100.00	-5835.00	0.00	-5935.00	0.00	-100.00	0.00	0.00
2 Jun-06	5490.00	100.00	-5390.00	0.00	-5490.00	0.00	-100.00	0.00	0.00
3 Jun-07	5006.00	100.00	-4906.00	0.00	-5006.00	0.00	-100.00	0.00	0.00
4 Jun-08	4938.00	100.00	-4838.00	0.00	-4938.00	0.00	-100.00	0.00	0.00
5 Jun-09	4888.00	100.00	-4788.00	0.00	-4888.00	0.00	-100.00	0.00	0.00
6 Jun-10	4840.00	100.00	-4740.00	0.00	-4840.00	0.00	-100.00	0.00	0.00
7 Jun-11	4840.00	50.00	-4790.00	0.00	-4840.00	0.00	-50.00	0.00	0.00
8 Out-03	4730.00	50.00	-4680.00	0.00	-4730.00	0.00	-50.00	0.00	0.00
9 UpperEastBasin	6694.00	100.00	-6594.00	0.00	-6694.00	0.00	-100.00	0.00	0.00

Junction Results

SN Element ID	Peak Inflow	Peak Lateral	Max HGL Elevation	Max HGL Depth	Max Surcharge		Average HGL Elevation	Average HGL Depth	Time of Max HGL	Time of Peak	Total Flooded	Total Time Flooded
		Inflow	Attained	Attained	Depth	Attained	Attained	Attained	Occurrence	Flooding		
					Attained					Occurrence		
	(cfs)	(cfs)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(days hh:mm)	(days hh:mm)	(ac-in)	(min)
1 Jun-05	107.74	0.00	5936.52	1.52	0.00	798.48	5935.05	0.05	0 00:25	0 00:00	0.00	0.00
2 Jun-06	0.00	0.00	5490.00	0.00	0.00	800.00	5490.00	0.00	0 00:00	0 00:00	0.00	0.00
3 Jun-07	484.42	484.42	5007.73	1.73	0.00	398.27	5006.03	0.03	0 00:18	0 00:00	0.00	0.00
4 Jun-08	407.46	107.34	4939.51	1.51	0.00	398.49	4938.03	0.03	0 00:23	0 00:00	0.00	0.00
5 Jun-09	1188.80	797.16	4891.29	3.29	0.00	296.71	4888.08	0.08	0 00:28	0 00:00	0.00	0.00
6 Jun-10	1103.02	0.00	4858.77	18.77	0.00	281.23	4840.50	0.50	0 00:33	0 00:00	0.00	0.00
7 Jun-11	624.44	5.02	4853.46	13.46	0.00	36.54	4844.82	4.82	0 01:23	0 00:00	0.00	0.00
8 Out-03	602.03	0.00	4733.00	3.00	0.00	0.00	4732.96	2.96	0 00:10	0 00:00	0.00	0.00
9 UpperEastBasin	165.57	165.57	6694.15	0.15	0.00	199.85	6694.00	0.00	0 00:12	0 00:00	0.00	0.00

Channel Input

SN Element ID	Length	Inlet Invert			Outlet Invert		Average Slope		Height	Width	Manning's Roughness	Entrance Losses	Exit/Bend Losses		Initial Flap Flow Gate
		Elevation	Offset	Elevation	Offset										
	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(%)		(ft)	(ft)					(cfs)
1 Link-03	10270.00	6694.00	0.00	5935.00	0.00	759.00	7.3900	Trapezoidal	200.000	1200.000	0.0400	0.5000	0.5000	0.0000	0.00 No
2 Link-04	4132.00	5935.00	0.00	5490.00	0.00	445.00	10.7700	Trapezoidal	800.000	3240.000	0.0400	0.5000	0.5000	0.0000	0.00 No
3 Link-05	4753.00	5490.00	0.00	5006.00	0.00	484.00	10.1800	Trapezoidal	225.000	1390.000	0.0400	0.5000	0.5000	0.0000	0.00 No
4 Link-06	3804.00	5006.00	0.00	4938.00	0.00	68.00	1.7900	Trapezoidal	400.000	2440.000	0.0400	0.5000	0.5000	0.0000	0.00 No
5 Link-07	1770.00	4938.00	0.00	4888.00	0.00	50.00	2.8200	Trapezoidal	300.000	1840.000	0.0400	0.5000	0.5000	0.0000	0.00 No
6 Link-08	4753.00	4888.00	0.00	4840.00	0.00	48.00	1.0100	Trapezoidal	300.000	1840.000	0.0400	0.5000	0.5000	0.0000	0.00 No
7 Link-09	3500.00	4840.00	0.00	4840.00	0.00	0.00	0.0000	Trapezoidal	50.000	700.000	0.0400	0.5000	0.5000	0.0000	0.00 No
8 Link-10	2594 00	4840 00	0.00	4730.00	0.00	110 00	4 2400	Trapezoidal	3 000	268 000	0.0400	0.5000	0.5000	0.0000	0.00 No

Channel Results

SN Element ID	Peak Flow	Time of Peak Flow	Design Flow Capacity	Peak Flow/ Design Flow	Peak Flow Velocity		Peak Flow Depth			Froude Reported Number Condition
		Occurrence		Ratio				Total Depth		
								Ratio		
	(cfs)	(days hh:mm)	(cfs)		(ft/sec)	(min)	(ft)		(min)	
1 Link-03	107.74	0 00:25	40096768.26	0.00	4.74	36.11	0.08	0.00	0.00	
2 Link-04	0.00	0 00:00	813440873.53	0.00	0.00		0.76	0.00	0.00	
3 Link-05	0.00	0 00:00	43773442.64	0.00	0.00		0.00	0.00	0.00	
4 Link-06	407.46	0 00:23	82279903.09	0.00	11.54	5.49	1.52	0.00	0.00	
5 Link-07	401.30	0 00:26	48722679.32	0.00	12.84	2.30	1.32	0.00	0.00	
6 Link-08	1103.02	0 00:33	29131946.60	0.00	11.21	7.07	3.06	0.01	0.00	
7 Link-09	624.44	0 01:23	6215.06	0.10	0.22	265.15	9.53	0.19	0.00	
8 Link-10	602.03	0 01:33	12056.80	0.05	4.81	8.99	0.50	0.17	0.00	

Attachment F

Hydraflow Express

Existing Channel Conditions

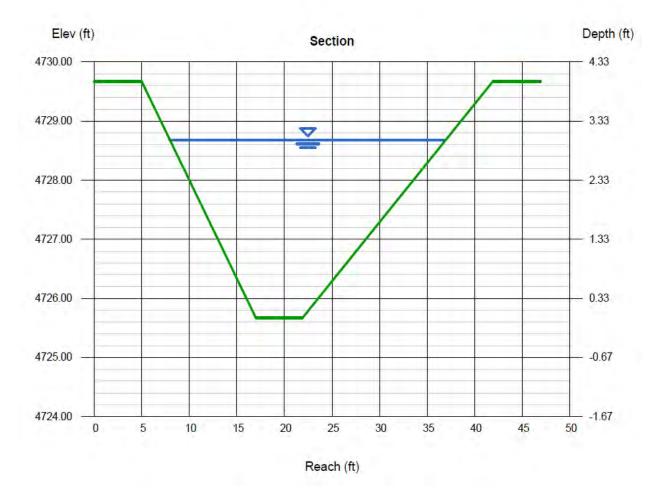
For the 10-year and 100-year Events

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Sunday, Feb 24 2019

Existing Upstream Channel - 10Yr

Trapezoidal		Highlighted	
Bottom Width (ft)	= 4.90	Depth (ft)	= 3.01
Side Slopes (z:1)	= 3.00, 5.00	Q (cfs)	= 300.00
Total Depth (ft)	= 4.00	Area (sqft)	= 50.99
Invert Elev (ft)	= 4725.67	Velocity (ft/s)	= 5.88
Slope (%)	= 1.00	Wetted Perim (ft)	= 29.77
N-Value	= 0.036	Crit Depth, Yc (ft)	= 2.69
		Top Width (ft)	= 28.98
Calculations		EGL (ft)	= 3.55
Compute by:	Known Q		
Known Q (cfs)	= 300.00		

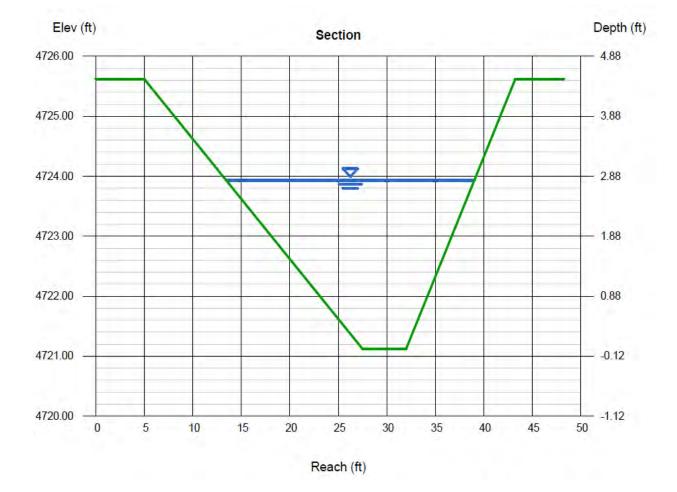


Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Sunday, Feb 24 2019

Existing Downstream Channel - 10 Yr Storm

Trapezoidal		Highlighted	
Bottom Width (ft)	= 4.50	Depth (ft)	= 2.81
Side Slopes (z:1)	= 5.00, 2.50	Q (cfs)	= 300.00
Total Depth (ft)	= 4.50	Area (sqft)	= 42.26
Invert Elev (ft)	= 4721.12	Velocity (ft/s)	= 7.10
Slope (%)	= 1.50	Wetted Perim (ft)	= 26.39
N-Value	= 0.035	Crit Depth, Yc (ft)	= 2.78
		Top Width (ft)	= 25.57
Calculations		EGL (ft)	= 3.59
Compute by:	Known Q		
Known Q (cfs)	= 300.00		

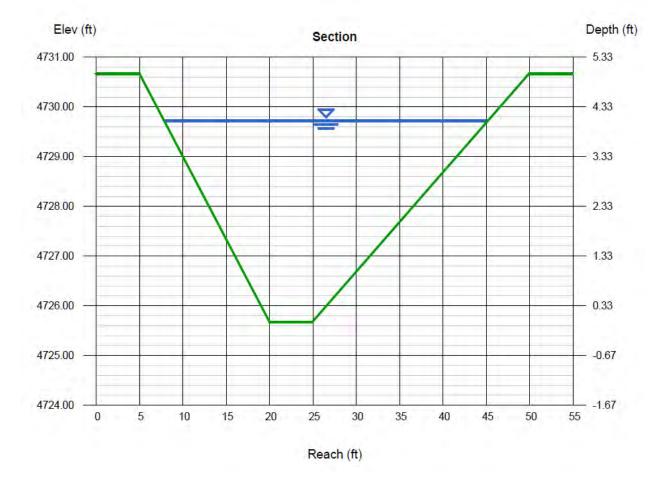


Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Sunday, Feb 24 2019

Existing Upstream Channel - 100Yr

Trapezoidal		Highlighted	
Bottom Width (ft)	= 4.90	Depth (ft)	= 4.05
Side Slopes (z:1)	= 3.00, 5.00	Q (cfs)	= 600.00
Total Depth (ft)	= 5.00	Area (sqft)	= 85.45
Invert Elev (ft)	= 4725.67	Velocity (ft/s)	= 7.02
Slope (%)	= 1.00	Wetted Perim (ft)	= 38.36
N-Value	= 0.036	Crit Depth, Yc (ft)	= 3.70
		Top Width (ft)	= 37.30
Calculations		EGL (ft)	= 4.82
Compute by:	Known Q		
Known Q (cfs)	= 600.00		

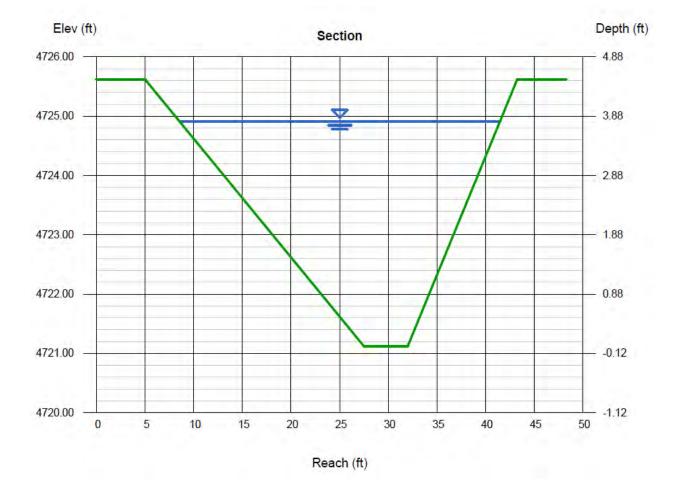


Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Sunday, Feb 24 2019

Existing Downstream Channel - 100 Yr Storm

Trapezoidal		Highlighted	
Bottom Width (ft)	= 4.50	Depth (ft)	= 3.79
Side Slopes (z:1)	= 5.00, 2.50	Q (cfs)	= 600.00
Total Depth (ft)	= 4.50	Area (sqft)	= 70.92
Invert Elev (ft)	= 4721.12	Velocity (ft/s)	= 8.46
Slope (%)	= 1.50	Wetted Perim (ft)	= 34.03
N-Value	= 0.035	Crit Depth, Yc (ft)	= 3.82
		Top Width (ft)	= 32.92
Calculations		EGL (ft)	= 4.90
Compute by:	Known Q		
Known Q (cfs)	= 600.00		



Attachment G

Hydraflow Express Culvert Report

Proposed Design – 10 Year Storm

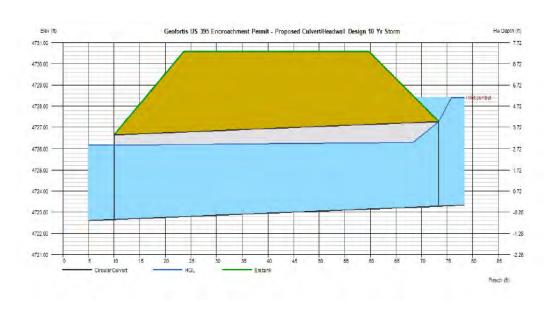
Culvert Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Sunday, Feb 24 2019

Geofortis US 395 Encroachment Permit - Proposed Culvert/Headwall Design 10 Yr Storr

Invert Elev Dn (ft)	= 4722.65	Calculations	
Pipe Length (ft)	= 63.38	Qmin (cfs)	= 300.00
Slope (%)	= 0.99	Qmax (cfs)	= 300.00
Invert Elev Up (ft)	= 4723.28	Tailwater Élev (ft)	= (dc+D)/2
Rise (in)	= 48.0		100
Shape	= Circular	Highlighted	
Span (in)	= 48.0	Qtotal (cfs)	= 300.00
No. Barrels	= 3	Qpipe (cfs)	= 300.00
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Corrugate Metal Pipe	Veloc Dn (ft/s)	= 8.55
Culvert Entrance	= Headwall	Veloc Up (ft/s)	= 9.80
Coeff. K,M,c,Y,k	= 0.0078, 2, 0.0379, 0.69, 0.5	HGL Dn (ft)	= 4726.16
		HGL Up (ft)	= 4726.31
Embankment		Hw Elev (ft)	= 4728.42
Top Elevation (ft)	= 4730.60	Hw/D (ft)	= 1.29
Top Width (ft)	= 36.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 24.00		



Attachment H

Hydraflow Express Culvert Report

Proposed Design – 100 Year Storm

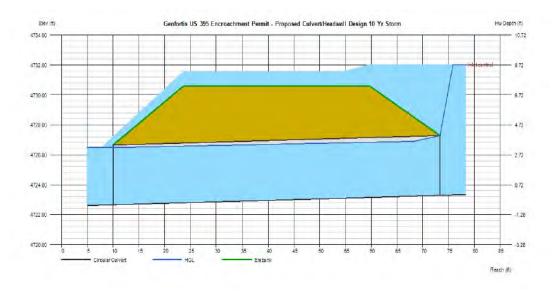
Culvert Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Sunday, Feb 24 2019

Geofortis US 395 Encroachment Permit - Proposed Culvert/Headwall Design 100 Yr Stc

Invert Elev Dn (ft)	= 4722.65	Calculations	
Pipe Length (ft)	= 63.38	Qmin (cfs)	= 600.00
Slope (%)	= 0.99	Qmax (cfs)	= 600.00
Invert Elev Up (ft)	= 4723.28	Tailwater Élev (ft)	= (dc+D)/2
Rise (in)	= 48.0		
Shape	= Circular	Highlighted	
Span (in)	= 48.0	Qtotal (cfs)	= 600.00
No. Barrels	= 3	Qpipe (cfs)	= 474.20
n-Value	= 0.012	Qovertop (cfs)	= 125.80
Culvert Type	= Circular Corrugate Metal Pipe	Veloc Dn (ft/s)	= 12.77
Culvert Entrance	= Headwall	Veloc Up (ft/s)	= 13.12
Coeff. K,M,c,Y,k	= 0.0078, 2, 0.0379, 0.69, 0.5	HGL Dn (ft)	= 4726.48
		HGL Up (ft)	= 4726.94
Embankment		Hw Elev (ft)	= 4732.02
Top Elevation (ft)	= 4730.60	Hw/D (ft)	= 2.18
Top Width (ft)	= 36.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 24.00		



Attachment I

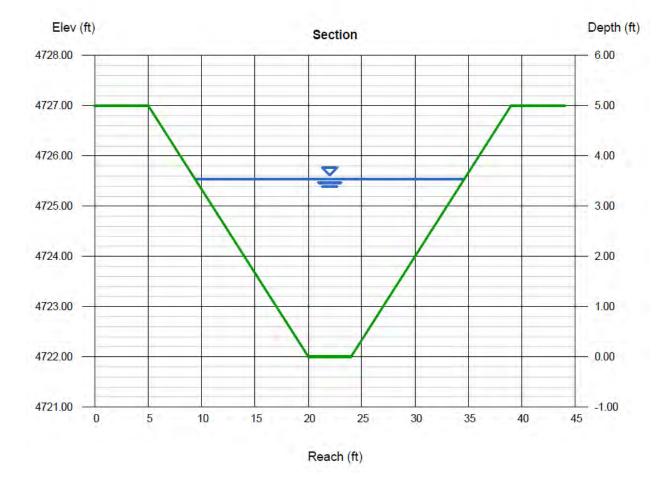
Hydraflow Express Channel Report
Proposed Channel Conditions
For the 10-year and 100-year Events

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Sunday, Feb 24 2019

Proposed Downstream Channel - 10Yr Storm

	Highlighted	
4.00	Depth (ft)	= 3.54
3.00, 3.00	Q (cfs)	= 300.00
5.00	Area (sqft)	= 51.75
4722.00	Velocity (ft/s)	= 5.80
1.00	Wetted Perim (ft)	= 26.39
0.040	Crit Depth, Yc (ft)	= 3.03
	Top Width (ft)	= 25.24
	EGL (ft)	= 4.06
own Q		
300.00		
(3.00, 3.00 5.00 4722.00 1.00 0.040	3.00, 3.00 Q (cfs) 5.00 Area (sqft) 4722.00 Velocity (ft/s) 1.00 Wetted Perim (ft) 0.040 Crit Depth, Yc (ft) Top Width (ft) EGL (ft)



Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Sunday, Feb 24 2019

Proposed Downstream Channel - 100Yr Storm

Trapezoidal		Highlighted	
Bottom Width (ft)	= 4.00	Depth (ft)	= 4.75
Side Slopes (z:1)	= 3.00, 3.00	Q (cfs)	= 600.00
Total Depth (ft)	= 5.00	Area (sqft)	= 86.69
Invert Elev (ft)	= 4722.00	Velocity (ft/s)	= 6.92
Slope (%)	= 1.00	Wetted Perim (ft)	= 34.04
N-Value	= 0.040	Crit Depth, Yc (ft)	= 4.17
		Top Width (ft)	= 32.50
Calculations		EGL (ft)	= 5.49
Compute by:	Known Q		
Known Q (cfs)	= 600.00		

